# Alicja Nejman, Irena Kamińska, Patrycja Giesz, Małgorzata Cieślak

# Thermal Stability of Polyester Fabric with Polyacrylic Coatings

**DOI:** 10.5604/12303666.1152734

Textile Research Institute, Scientific Department of Unconventional Technologies and Textiles, ul. Brzezinska 5/15, 92-103 Łódź, Poland E-mail address: cieslakm@iw.lodz.pl

#### Abstract

The aim of the study was to assess the thermal properties of polyester (PET) woven fabrics with unmodified (PET/AC) and flame-retardant modified (PET/AC/FR) polyacrylic coatings, before and after 1, 5, 10 & 15 washes. Differential scanning calorimetry DSC and thermogravimetric TG/DTG analyses were carried out in order to investigate the thermal processes. To evaluate the effects of the modifications and washing treatment, the scanning electron microscopy SEM/EDS technique was used. The flame-retardant modification caused that the melting enthalpy and the initial thermal degradation temperature decreased and the thermal degradation heat increased. The washing of PET/AC and PET/AC/FR fabrics caused an increase in the melting enthalpy by approximately 12% and 63% and a decrease in thermal degradation heat by about 2% and 15%, respectively. It was found that the flame-retardants were rinsed out from the coating after the fifth wash.

**Key words:** textiles, polymers, coating, flame-retardant, DSC, TG/DTG.

with different functional materials e.g. flame-retardant agents, antistatic, bioactive, UV protection, etc. [7 - 11]. Textile materials made of conventional natural or synthetic fibres may pose a potential fire hazard (eg. in buildings of public use). Conventional polyester such as poly(ethylene terephthalate) (PET) melt and drip tend to degrade and pyrolysis under the influence of the self-sustaining combustion process in fire conditions [7]. This disadventage limits their use in many areas [1], therefore PET materials are modified with flame retardant agents,

**Table 1.** Characteristics of coating pastes; \* The amount of thickener Setaprint (PTL) was added to obtain the appropriate viscosity of the paste.

Paste compositions	Weight percentage, wt%			
r date compositions	flame-re	tardants		
	without	with		
Dicrylan AC	97.8	54.9		
Rustol BXB	0.2	0.1		
Pericoat Crosslinker MV	2.0	1.1		
Setaprint (PTL)	х	*		
Pekoflam TC 303	- 27.4			
Pekoflam PES	-	16.5		
Viscosity dPas	115	103		

Table 2. Characteristic of fabrics studied.

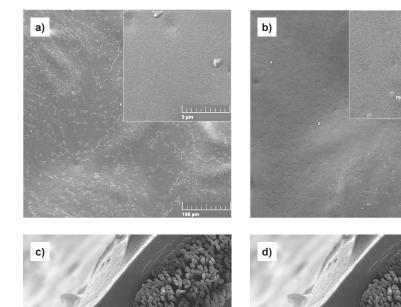
Fabric	Raw	With unmodified coating	With flame- retardant coating	
Mass per unit area, g/m <sup>2</sup>		94	145	218
Mass per unit area of dry coating, g/m <sup>2</sup>			51	124
The flame retardant content, g/m <sup>2</sup>		-	54	
	1 wash	-	145	185
Mass per unit area after	5 wash		145	156
washing treatment, g/m <sup>2</sup>	10 wash		145	155
	15 wash		145	156

Table 3. List of test samples; \*R-resin, \*\*f-film.

Samples	Symbol		
Cross-linked polyacrylic resin Dicrylan AC - film	AC/R*/f**		
Flame-retardant Pekoflam PES - liquid	FR1		
Flame-retardant Pekoflam TC 303 - powder	FR2		
Crosslinked coating - film	AC/f		
Crosslinked coating with flame-retardants - film	AC/FR/f		
Raw PET fabric	PET		
PET fabric impregnated before unmodified coating	PET/B1		
PET fabric impregnated before flame-retardant coating	PET/B2		
PET fabric with unmodified coating	PET/AC		
PET fabric with flame-retardant coating	PET/AC/FR		
PET fabric with unmodified coating after 1, 5, 10 and 15 washes	PET/AC/1;5;10;15		
PET fabric with flame-retardant coating after 1, 5, 10 and 15 washes	PET/AC/FR/1;5;10;15		

## Introduction

The aim of the functional modification of textile materials is to change their physical, chemical and biological properties [1 - 6]. One of the ways to modify textile materials is the application of polymer coatings [5]. In order to achieve the properties of the final product intended, it is important to choose appropriate textile structures and film-forming materials. Many factors e.g. the possibility of film formation, adhesion, flexibility, and resistance to abrasion, water, solvents, hydrolysis, UV radiation, thermal plasticity, melting, thermal resistance, etc. [6] have an influence on the choice of the basic film-forming polymer. Polyacrylates used to coat textiles are often modified



**Figure 1.** SEM images of coated fabrics (PET/AC): a) surface of unmodified coating before and b) after 15 washes, c) the cross-section of coated fabric before and d) after 15 washes.

chosen for raising the temperature of ignition, and for inhibiting or retarding the thermal degradation process of textile materials. For safety reasons, flammability properties should be maintained for the lifetime of the product.

The aim of the study was to assess the thermal properties of polyester (PET) fabrics with unmodified and flame-retardant modified polyacrylate coatings before and after washing treatment. The fabric was modified by a coating technique commonly used, and which met the criteria of flammability tests for curtains. Differential scanning calorimetry DSC andthermogravimetric TG/DTG analyses were carried out in order to investigate the thermal processes. To evaluate the effects of the modifications and washing treatment the scanning electron microscopy SEM/EDS technique was used.

# Experimental

#### Materials

Commercial polyester woven fabric made of poly(ethylene terephthalate) (PET) with a plain weave,warp density of 390/10 cm and weft density of 320/10

cm was used. Before coating with polymer paste without flame retardant agents, the raw fabric was impregnated with a bath (B1) containing 20 g/l Periguard UFC (Dr. Petra, Germany), 3 g/l Periguard EXT (Dr. Petra, Germany), 10 g/l isopropyl alcohol and acetic acid. Before coating with the paste containing flame-retardant agents, the raw fabric was impregnated with a bath (B2) containing 12 g/l Periguard UFC (Dr. Petra, Germany), 100 g/l Pekoflam PES (Clariant, Switzerland), 10 g/l isopropyl alcohol and ammonia.

On the basis of polyacrylic polymer, two types of coating pastes were prepared, with and without flame-retardants (FR) (Table 1). For the basic paste, Dicrylan AC (Huntsman, Germany), Rustol BXB (Rudolf, Germany), Pericoat Crosslinker MV (Dr. Petry, Germany), and Setaprint PTL (Setas Kimya) were used, and as flame-retardants Pekoflam TC 303 - inorganic phosphorus compounds and Pekoflam PES - organic phosphorus compounds (Clariant, Switzerland) were applied. The fabric was coated on one side. Characteristics of fabrics studied are presented in Table 2. Table 3 summarizes all of test samples.

#### Methods

#### Film preparation

In order to obtain cross-linked films, a thin layer of resin and polymer pastes were poured on Petri dishes and dried in an oven at 110 °C for 4 hours.

#### Fabric impregnation

Before coating with polyacrylic paste without flame-retardants, the fabric was impregnated on a two-roll padder (Benz, Switzerland, rolles pressure of 3.5 daN/cm) with a bath B1 of 20 °C and dried at 100 °C at a rate of 1.5 m/min for 5 min.

Before coating with flame-retardant modified paste, the fabric was impregnated with a bath B2 of 20 °C (rolles pressure of 3 daN/cm), dried at 100 - 120 - 150 °C at a rate of 1.5 m/min for 3 min, thermal treated at 185 °C for 2 min, and then rinsed in water with 1 g/l Polyacrylic A at 60 °C (2 passages), and next in water at 60 °C (1 passage) and 40 °C (1 passage).

#### Fabric coating

The fabrics were coated using a coating machine, Werner Mathis AG (Switzerland) with an air knife (distance of 0.1 mm), dried at 100 - 120 °C at a rate of 1 m/min for 10 min and thermal treated at 160 °C for 2 min.

# Washing

Samples of coated fabrics were washed in a automatic washing machine - Vascator FOM71 MP LAB (Electrolux, Switzerland) at 40 °C and dried (according to PN-EN ISO 6330: 2012, the program 4N).

# Instrumental techniques

SEM/EDS analysis

Microscopic analysis SEM/EDS was carried out using the scanning electron microscope VEGA 3 (Tescan, Czech Republic) with a X-ray microanalyzer - EDS INCA (Oxford Analytical Instruments, UK) at  $500\times$  magnification. SEM images, EDS X-ray SmartMaps on a microarea of 46 650  $\mu$ m² and a EDS Sum Spectrum were obtained. The average weight percentage of elements was determined on the basis of the EDS Sum Spectrum obtained for three different microareas of each sample.

#### DSC analysis

A study of thermal properties was performed using a differential scanning calorimeter -DSC 204 F1 Phoenix (Netzsch,

Germany). All samples were tested in a ceramic crucible with a volume of 85 µl in a nitrogen atmosphere (gas flow of 25 ml/min), at a heating rate 10 °C/min in the range of 20 - 600 °C. Three samples of each material with masses of 5 - 16 mg were examined. Based on the DSC thermograms the melting enthalpy (ΔH<sub>m</sub>), the heat of thermal degradation  $(\Delta H_{Deg.})$ , the initial  $(T_{Onset})$  and final (T<sub>End</sub>) temperature of melting and the thermal degradation and temperature at the peak maxima (T<sub>Max</sub>) of the raw and coated fabrics were determined. The initial  $(T_{Onset})$ , final  $(T_{End})$  and peak maxima (T<sub>Max</sub>) temperatures of the thermal degradation and the heat of thermal degradation ( $\Delta H_{Deg.}$ ) of films and flameretardant agents were determined.

# TG/DTG analysis

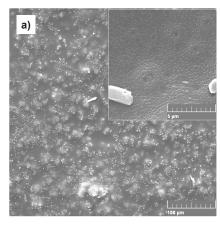
TG/DTG analysis was performed using a thermogravimetric analyser TG 209 F1 Libra (Netzsch, Germany). All samples were tested in a ceramic crucible with a volume of 85  $\mu$ l in a nitrogen atmosphere (gas flow of 25 ml/min.), with a heating rate of 10 °C/min in the range of 30 - 600 °C. Three samples of each materials with masses of 5 - 16 mg were examined. The weight loss of samples in the temperature range of peaks occurrence on the DTG curves and the initial ( $T_{Onset}$ ), final ( $T_{End}$ ) and the peaks maxima ( $T_{Max}$ ) temperature of the thermal degradation were determined.

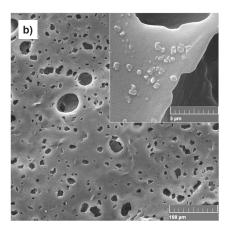
# Results and discussion

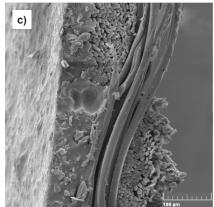
#### **SEM/EDS** analysis

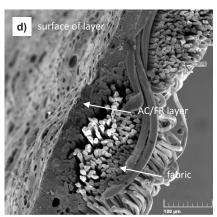
Microscopic images of the coated fabrics are presented in *Figures 1* and 2. Figures 1.a and 1.c show the fabric with unmodified coating (PET/AC) before the washing treatment and Figures 1.b and 1.d - after 15 washes. The coating before washing forms a continuous film with fine pores. After 15 washings (Figures 1b and 1d) there were no defects in the coating and pores are clearly smaller. Figures 2.a and 2.c show the flame-retardant fabric (PET/AC/FR) before the washing with visible agglomerates of flame-retardant agents. After 15 washings (Figures 2.b and 2.d) a plurality of recesses/open pores are present, which may be the result of removed flame-retardant agents.

On the basis of X-ray spectra emitted from the flame-retardant agents, it was found that FR1 contains C, O, P and S, and FR2 contains C, N, O & P (*Figure 3*).









**Figure 2.** Figure 2. SEM images of fabrics with flame-retardant coating (PET/AC/FR): a) surface of modified coating before and b) after 15 washes, c) the cross-section of coated fabric before and d) after 15 washes.

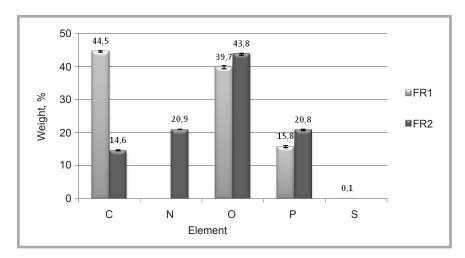


Figure 3. Weight percentage of elements in flame-retardant agents FR1 and FR2.

**Table 4.** Weight percentage of elements in the flame-retardant coating on the fabric before and after 1, 5, 10 & 15 washes.

F1	Weight percentage, wt%							
Element	PET/AC/FR	PET/AC/FR/ 1	PET/AC/FR/ 5	PET/AC/FR/ 10	PET/AC/FR/ 15			
С Κα	56.81	64.42	67.95	69.19	67.32			
Ν Κα	3.68	3.31	2.33	1.98	1.74			
Ο Κα	30.59	28.61	27.55	26.79	28.97			
Na Kα	-	0.44	1.16	1.32	1.36			
РΚα	8.78	3.10	0.90	0.60	0.50			
S Ka	0.14	0.11	0.11	0.11	0.10			

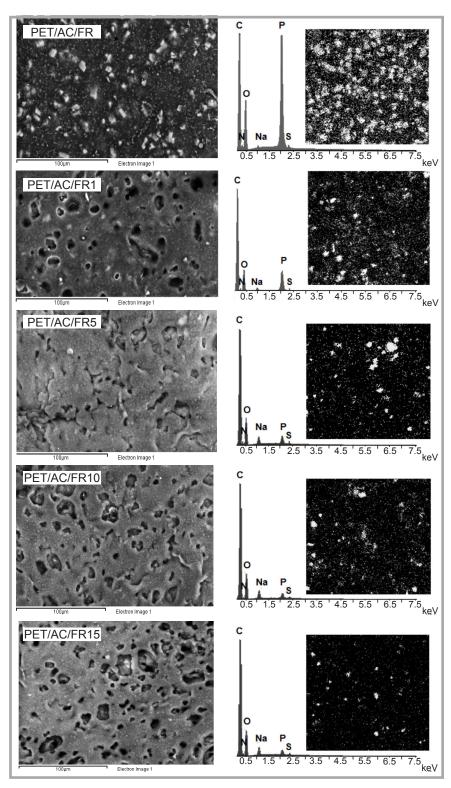


Figure 4. SEM images, X-ray SmartMaps of phosphorus and Sum Spectra for the flameretardant coating of fabric before and after the washing treatment.

**Table 5.** Results of DSC analysis for samples studied; a mean value  $\pm$  standard deviation,  ${}^bFR2$  thermal degradation process is exothermic; the table shows the absolute value of the heat of its thermal degradation  ${}^cFR=FR1+FR2$  in relation 2:1.

Sample	ΔH <sub>Deg</sub> , J/g	T <sub>Onset</sub> , °C	T <sub>End</sub> , °C	T <sub>Max1</sub> , °C	T <sub>Max2</sub> , °C
AC/R/f	345.8 ± 2.9a	375.2 ± 0.4	422.1 ± 1.3	397.3 ± 0.8	-
AC/f	342.6 ± 2.7	365.2 ± 0.7	424.2 ± 0.6	396.4 ± 0.7	-
FR1	562.7 ± 1.1	290.8 ± 1.7	344.9 ± 1.9	326.4 ± 0.8	-
FR2	147.0 ± 2.9b	345.3 ± 1.2	352.5 ± 2.1	349.6 ± 0.7	-
AC/FRc/f	325.4 ± 2.2	246.1 ± 0.7	402.7 ± 1.0	310.7 ± 1.6	383.7 ± 1.9

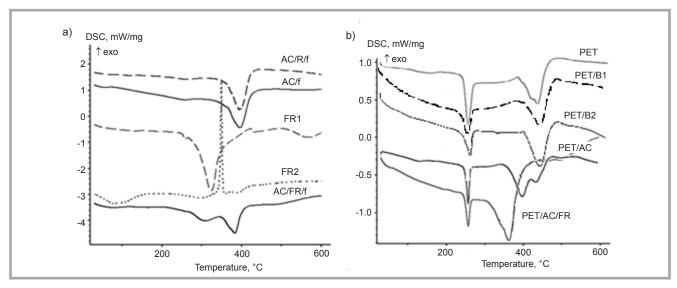
FR2 has 20.9 wt% of nitrogen, which is not present in FR1. The percentage of phosphorus is 15.8 wt% and 20.8 wt% in FR1 and FR2, respectively. In FR1 there is also present a small amount of sulphur.

**Table 4** shows the weight percentage of elements in the flame-retardant coating on the fabric before and after the washing treatment.

In the coating of PET/AC/FR fabric, C, N, O, P and S were found and the dominant elements are C, O & P. After washing, this coating contains additional Na (0.44 wt% to 1.36 wt%, increasing with the number of washes), which is residue after the washing treatment. The fabric coating with flame-retardants before washing has 8.78 wt% of phosphorus (Table 4), derived from FR1 and FR2 agents (Figure 3). The proportion of phosphorus in the flame-retardant coating decreases after subsequent washing treatments, from 3.10 wt% to 0.50 wt% (Table 4). The flame-retardant agents were rinsed during the washing treatment. Changes in the contents of phosphorus in the fabric coatings obtained by SmartMaps and X-ray spectra confirm the results of SEM image analysis (Figure 4).

#### **DSC** analysis

In Figure 5, DSC thermograms of all materials and fabrics used are presented. For the raw fabric (Figure 5.b) the endothermic melting peak with a maximum at 257.1  $\pm$  0.4 °C (*Table 6*) is visible, and the melting enthalpy is 52.1  $\pm$  0.9 J/g (*Figure 6*). The endothermic peak of thermal degradation reaches the maximum at  $442.9 \pm 0.9$  °C and the heat of thermal degradation amounted to  $115.6 \pm 0.9 \text{ J/g}$  (**Table 6**). A similar result was obtained by Lecomte et al. [12]. Preliminary impregnation of the fabrics before coating with unmodified paste (PET/B1) and flame-retardant paste (PET/B2) does not influence their degradation temperature changes in comparison with the raw fabric. For the impregnated PET/B1 sample an endothermic melting peak with a maximum at  $254.9 \pm 1.1$  °C is present (Table 6), and the melting enthalpy amounted to  $49.0 \pm 1.0 \text{ J/g}$  (*Figure 6*). The degradation of the PET/B1 sample takes place in a single step with the endothermic peak maximum at  $443.0 \pm 1.2$  °C and a heat of degradation of  $115.5 \pm 0.5 \,\mathrm{J/g}$ (Table 6). For the impregnated PET/B2 sample a endothermic melting peak with a maximum at  $255.0 \pm 1.0$  °C is pre-



**Figure 5.** DSC thermograms of a) cross-linked polyacrylic resin (AC/R/f), cross-linked polyacrylic coating (AC/f), flame-retardant agents (FR1, FR2), cross-linked flame-retardant coating (AC/FR/f), and b) raw fabric (PET), fabric impregnated before unmodified coating (PET/B1), fabric impregnated before flame-retardant coating (PET/B2), fabric with unmodified coating (PET/AC), fabric with flame-retardant coating (PET/AC/FR).

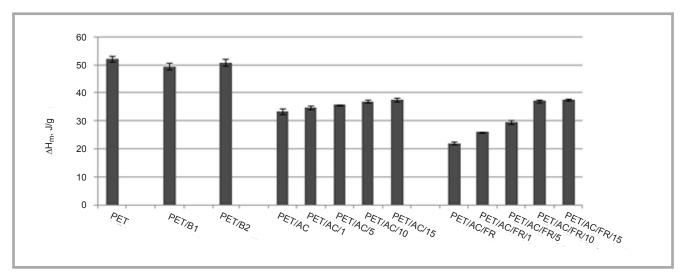


Figure 6. Melting enthalpy values of fabrics before and after the washing treatment.

**Table 6.** DSC results for fabrics before and after washing treatment; amean value  $\pm$  standard deviation.

0-			Melting process			Thermal degradation process				
Sample		T <sub>Onset</sub> , °C	T <sub>End</sub> , °C	T <sub>Max</sub> , °C	ΔH <sub>Deg</sub> , J/g	T <sub>Onset</sub> , °C	T <sub>End</sub> , °C	T <sub>Max1</sub> , °C	T <sub>Max2</sub> , °C	
ſ	PET	250.9 ± 0.9a	261.5 ± 0.7	257.1 ± 0.4	115.6 ± 0.9	403.7 ± 0.7	466.9 ± 0.9	442.9 ± 0.9	-	
PE	ET/B1	247.8 ± 0.4	260.7 ± 0.7	254.9 ± 1.1	115.5 ± 0.5	402.9 ± 0.5	465.9 ± 1.3	443.0 ± 1.2	-	
PE	ET/B2	249.1 ± 1.0	260.2 ± 0.5	255.0 ± 1.0	115.1 ± 0.7	405.1 ± 0.3	468.1 ± 1.0	444.0 ± 1.0	-	
	PET/AC	251.1 ± 0.3	264.5 ± 0.4	258.7 ± 0.3	198.3 ± 1.5	371.2 ± 1.0	465.2 ± 0.9	398.1 ± 0.7	434.6 ± 0.5	
fabric with	PET/AC/1	251.4 ± 0.2	265.1 ± 0.3	258.8 ± 0.5	197.5 ± 1.6	363.7 ± 1.1	469.5 ± 0.8	397.3 ± 0.6	434.9 ± 0.8	
unmodified	PET/AC/5	251.6 ± 0.5	265.4 ± 0.3	259.4 ± 0.4	197.3 ± 1.1	367.2 ± 1.4	470.3 ± 0.5	399.3 ± 1.1	434.9 ± 0.5	
coating	PET/AC/10	251.7 ± 1.8	265.6 ± 1.0	260.0 ± 1.1	195.6 ± 2.1	365.2 ± 0.8	478.2 ± 1.2	397.5 ± 0.2	438.3 ± 0.4	
	PET/AC/15	251.6 ± 1.3	265.8 ± 0.3	259.8 ± 0.9	193.9 ± 1.5	364.3 ± 0.9	471.3 ± 1.4	399.0 ± 0.7	438.4 ± 0.8	
	PET/AC/FR	249.0 ± 0.5	262.7 ± 0.4	257.7 ± 1.2	242.9 ± 3.0	327.0 ± 2.7	390.3 ± 1.0	362.6 ± 0.6	-	
fabric with	PET/AC/FR/1	247.2 ± 1.2	262.7 ± 0.9	257.9 ± 1.1	230.8 ± 2.1	344.5 ± 0.8	389.4 ± 0.8	376.6 ± 1.3	-	
flame- retardant coating	PET/AC/FR/5	250.8 ± 0.3	264.8 ± 0.4	259.8 ± 1.0	207.6 ± 2.6	376.4 ± 2.0	472.1 ± 1.0	403.0 ± 1.0	430.4 ± 0.6	
	PET/AC/FR/10	250.5 ± 0.6	264.7 ± 1.1	259.8 ± 0.7	207.3 ± 3.2	387.6 ± 1.2	467.5 ± 0.5	403.1 ± 0.5	432.8 ± 0.7	
	PET/AC/FR/15	250.3 ± 0.4	263.6 ± 1.3	260.7 ± 0.9	207.6 ± 1.5	380.2 ± 1.6	470.9 ± 0.5	404.8 ± 0.9	437.3 ± 0.4	

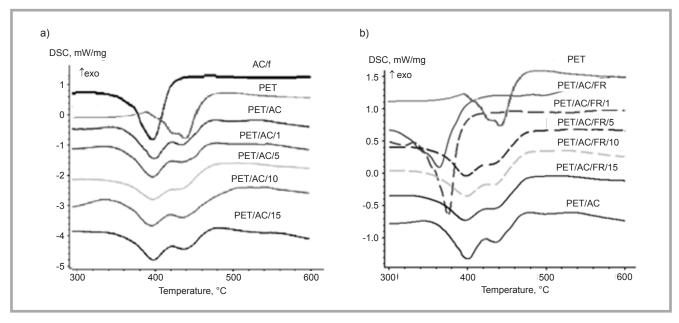


Figure 7. DSC thermograms of thermal degradation of a) fabrics with unmodified coating and b) fabrics with flame-retardant coating, before and after the washing treatment.

sent (*Table 6*), and the melting enthalpy amounted to  $50.87 \pm 1.2 \text{ J/g}$  (*Figure 6*). The degradation of this sample takes place in a single step with the endothermic peak maximum at 444.0 ± 1.0 °C and with a heat of degradation of 115.1  $\pm$  0.7 J/g (*Table 6*). Degradation of the cross-linked polyacrylic resin (AC/R/f) takes place in the range of  $375.2 \pm 0.4$  °C - 422.1  $\pm$  1.3 °C with  $T_{\mbox{\scriptsize Max}1}$  at 397.3 ± 0.8 °C (Table 5) and with a heat of degradation of 345.8  $\pm$  2.9 J/g. Crosslinked polyacrylic coating (AC/f) is degraded in the temperature range of 365.2  $\pm$  0.7 °C - 424.2 $\pm$ 0.6°C with  $T_{Max1}$  at  $396.4 \pm 0.7$  °C and with a heat of degradation of  $342.6 \pm 2.7$  J/g (*Table 5*). The mass per unit area of PET/AC fabric is 145 g/m<sup>2</sup> (Table 2), including raw fabric of mass 94 g/m<sup>2</sup> (65 wt%) and crosslinked coating (AC/f) of mass 51 g/m<sup>2</sup> (35 wt%) (Table 2). It can be concluded that the value of thermal degradation heat of PET/AC fabric is the total value of the heat of textile material and coating components. Flame-retardants FR1 and FR2 are degraded at much lower temperatures: FR1 at  $290.8 \pm 1.7$  °C with the endothermic peak at  $326.4 \pm 0.8$  °C and FR2  $345.3 \pm 1.2$  °C with the exothermic peak at  $349.6 \pm 0.7$  °C. Thermal degradation of the cross-linked flame-retardant coating (AC/FR/f) is two-step in the range 246.1  $\pm$  0.7 °C - 402.7  $\pm$  1.0 °C with  $T_{Max1}$  at 310.7 ± 1.6 °C and  $T_{Max2}$ at  $383.7 \pm 1.9$  °C and with a heat of degradation of  $325.4 \pm 2.2$  J/g (*Table 5*, see page 76).

The unmodified polyacrylic coating causes an increase in the melting temperature T<sub>Max</sub> of about 1.5 °C (*Figure 5.b*, *Table 6*, see page 77), a decrease in the melting enthalpy of about 19 J/g (*Figure 6*), and an decrease in the initial temperature of degradation of about 32°C in comparison with the raw fabric. The degradation of unwashed PET/AC fabric takes place in two steps with the endothermic peaks of the textile material and coating (*Table 6*).

The melting temperature  $T_{Max}$  of PET/AC/FR fabric decreased by 1 °C in comparison with PET/AC fabric (*Figure 5.b, Table 6*). The melting enthalpy is also lower and amounts to  $22.0 \pm 0.6$  J/g (*Figure 6*). The beginning of thermal degradation occurs at a temperature lower by 44.2 °C. The degradation heat of the PET/AC/FR fabric (*Table 6*), as in the case of PET/AC fabric, is the total value of the heat of two components: the textile material (43 wt%) and crosslinked flame-resistant coating AC/FR/f (57 wt%) (*Table 2*).

As follows from the values shown in *Table 6*, the washing treatment of PET/AC fabric did not affect changes in the initial temperature of the melting process. The temperature at the maximum of the melting peak increased by about 1 °C. For PET/AC/FR fabric, after 15 washes the initial melting temperature and peak maximum increased, respectively, by 1.3 °C and 3 °C. Multiple washing of PET/AC and PET/AC/FR fabrics caused an increase in their melting enthalpies

(*Figure 6*). After 15 washes, the values of the melting enthalpy for PET/AC/15 increased by 4.2 J/g and for PET/AC/FR/15 by 15.6 J/g.

For PET/AC/15 fabric the initial temperature of degradation Tonset decreased by 6.9 °C, and the final temperature T<sub>End</sub> increased by 5.1 °C (Table 6, Figure 7.a). The temperature T<sub>Max1</sub> and T<sub>Max2</sub> increased by about 1 °C and 4 °C, respectively, and the value of the decomposition heat decreased by about 4.5 J/g. After the 1st wash the mass per unir area of PET/AC/1 fabric had not changed (Table 2). For PET/AC/FR/1 fabric the initial temperature and maximum peak temperature of degradation increased by 17.5 °C and 14 °C, respectively, and the degradation heat decreased by 12 J/g. For both PET/AC/FR and PET/AC/FR1 fabrics, on the DSC thermograms there is no visible characteristic peak of PET component degradation, which indicates that the degradation of PET fabrics occurred simultaneously with the degradation of the flame-resistant coating (Figure 7.b). After the 5th wash there is no visible characteristic peak of the flameresistant coating (Figure 7.b), and the mass per unit area of PET/AC/FR/5 (Table 2) is reduced by 28%. For this fabric a characteristic peak of the degradation of the unmodified coating is present, which indicates a total or partial flameretardant rinse, confirmed by the results of the SEM/EDS analysis (Table 4). After 5, 10 and 15 washes, characteristic peaks of PET/AC fabric degradation

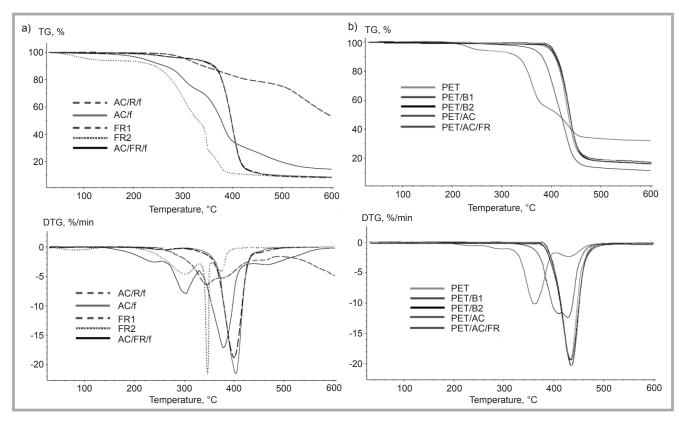


Figure 8. TG/DTG thermograms of thermal degradation of a) cross-linked polyacrylic resin (AC/R/f), cross-linked polyacrylic coating (AC/f), flame-retardant agents (FR1, FR2), and cross-linked flame-retardant coating (AC/FR/f); b) raw fabric (PET), fabric impregnated before unmodified coating (PET/B1), fabric impregnated before flame-retardant coating (PET/B2), fabric with unmodified coating (PET/AC/FR).

are present. Values of the initial and final temperatures and the endothermic peak maxima of degradation increased and the heat of degradation decreased by 35 J/g compared to the unwashed PET/AC/FR fabric (*Table 6*).

# TG/DTG analysis

Thermal degradation of the raw fabric occurs in a single step with Tonset at  $395.4 \pm 1.1$  °C and  $T_{Max1}$  431.1 ± 1.6 °C. A similar result was obtained by Lecomte et al. [12]. The weight loss for the raw fabric at  $T_{End}$  459.8  $\pm$  1.9 °C is 81.3  $\pm$  0.3% (Table 8, Figure 8.b). Preliminary impregnations before coating (PET/B1 and PET/B2) did not affect the degradation temperature changes in relation to the raw fabric. Thermal degradation of PET/B1 fabric starts at 396.1  $\pm$  1.8 °C and reaches a maximum of the endothermic peak at  $432.7 \pm 1.5$  °C, and the weight loss at  $T_{End}$  460.8 ± 1.2 °C is 80.2 ± 0.9%. Thermal degradation of PET/B2 fabric starts at  $394.9 \pm 0.8$  °C and reaches a maximum of the endothermic peak at  $432.5 \pm 0.5$  °C, and the weight loss at  $T_{End}$  458.3 ± 0.7 °C is 81.1 ± 0.7%.

Degradation of the cross-linked polyacrylic resin-film (AC/R/f) starts at  $T_{Onset}$ 

364.4  $\pm$  1.4 °C and proceeds in a single step, with a maximum of the endothermic peak at 406.0  $\pm$  1.2 °C (*Table 7*, *Figure 8.a*). The process ends at 424.6  $\pm$  1.2 °C with a weight loss of 88.2  $\pm$  1.1%. Similarly, in a single step the cross-linked unmodified coating – film (AC/f) is degrad-

ed, with a maximum of the endothermic peak at  $401.7 \pm 1.1$  °C. The process ends at  $423.4 \pm 0.4$  °C, at which the weight loss is  $83.4 \pm 0.9\%$ .

The degradation of flame-retardant agent FR1 occurs in two steps (*Figure 8.a*):

**Table 7.** TG/DTG analysis results for cross-linked polyacrylic resin-film (AC/R/f), cross-linked unmodified coating-film (AC/f), flame-retardants (FR1, FR2), and cross-linked flame-retardant coating-film (AC/FR/f);  $^b$ mean value  $\pm$  standard deviation.

		AC/R/f	AC/f	FR1	FR2	AC/FR/f
Step 1	T <sub>Onset</sub> , °C	364.4 ± 1.4b	368.2 ± 0.7	289.2 ± 0.8	245.4 ± 1.4	294.3 ± 2.1
	T <sub>Max1</sub> , °C	406.0 ± 1.2	401.7 ± 1.1	344.8 ± 0.9	304.0 ± 1.4	296.0 ± 2.5
Siep i	T End, °C	424.6 ± 1.2	423.4 ± 0.4	365.2 ± 1.3	332.1 ± 1.2	325.8 ± 2.3
	Residual weight, %	11.8 ± 1.1	16.6 ± 0.9	91.1 ± 0.5	49.4 ± 0.8	80.4 ± 1.2
	T <sub>Onset</sub> , °C	-	-	365.2 ± 1.3	332.1 ± 1.2	325.8 ± 2.3
Step 2	T <sub>Max2</sub> , °C	-	-	378.6 ± 0.4	$349.5 \pm 0.7$	382.2 ± 1.8
Siep 2	T <sub>End</sub> , °C	-	-	417.9 ± 1.4	357.5 ± 1.1	402.4 ± 1.1
	Residual weight, %	-	-	85.3 ± 0.9	24. 8 ± 0.6	51.5 ± 1.3
	T <sub>Onset</sub> , °C	-	-	-	357.5 ± 1.1	-
Step 3	T <sub>Max3</sub> , °C	-	-	-	$378.9 \pm 0.8$	-
Step 3	T <sub>End</sub> , °C	-	-	-	389.0 ± 1.5	-
	Residual weight, %	-	-	-	10.4 ± 1.3	-

**Table 8.** TG/DTG results for raw and impregnated fabrics before and after washes.

		PET	PET/B1	PET/B2
	T <sub>Onset</sub> , °C	395.4 ± 1.1b	396.1 ± 1.8	394.9 ± 0.8
Step 1	T <sub>Max</sub> , °C	431.1 ± 1.6	432.7 ± 1.5	432.5 ± 0.5
	T <sub>End</sub> , °C	459.8 ± 1.9	460.8 ± 1.2	458.3 ± 0.7
	Residual weight, %	18.7 ± 0.3	19.8 ± 0.9	18.9 ± 0.7

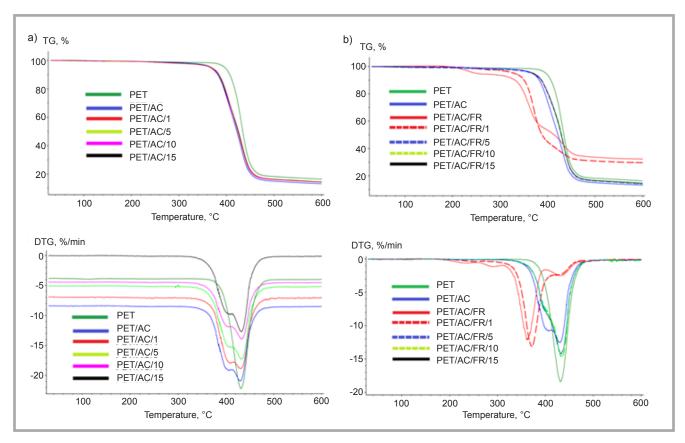


Figure 9. TG/DTG thermograms of a) fabrics with unmodified coating, and b) fabrics with flame-retardant coating, before and after washes.

with the beginning at  $289.2 \pm 0.8$  °C and with a weight loss at 600 °C of  $27.9 \pm 0.8$ %. For flame-retardant agent FR2 the thermal degradation process pro-

ceeds multistage. The weight loss at the final temperature of the third step -  $389.0 \pm 1.5$  °C is  $93.5 \pm 1.2$ %. Degradation of the cross-linked flame-retardant coat-

Table 9. TG/DTG results for fabrics with unmodified coating before and after washes.

		PET/AC	PET/AC/1	PET/AC/5	PET/AC/10	PET/AC/15
	T Onset 1, °C	376.0 ± 1.1b	375.6 ± 0.3	376.8 ± 1.0	374.2 ± 1.1	375.3 ± 0.2
Step 1	T <sub>Max 1</sub> , °C	405.6 ± 1.4	407.6 ± 1.1	407.7 ± 1.7	405.8 ± 1.0	405.0 ± 0.6
Step 1	T End 1, °C	414.8 ± 0.9	415.7 ± 1.5	415.2 ± 1.0	415.1 ± 0.8	415.7 ± 0.9
	Residual weight, %	59.9 ± 0.3	61.2 ± 0.6	63.6 ± 0.2	66.0 ± 0.7	66.8 ± 0.4
	T Onset 2, °C	414.8 ± 0.9	415.7 ± 1.5	415.2 ± 1.0	415.1 ± 0.8	415.7 ± 0.9
04 0	T <sub>Max 2</sub> , °C	430.1 ± 0.3	431.4 ± 1.2	431.9 ± 0.3	432.6 ± 1.3	432.0 ± 1.2
Step 2	T End 2, °C	472.4 ± 0.4	476.2 ± 0.5	476.8 ± 2.1	475.4 ± 0.5	474.5 ± 0.9
	Residual weight, %	16.5 ± 0.8	16.5 ± 0.7	16.8 ± 0.0	17.0 ± 0.6	14.8 ± 0.7

Table 10. TG/DTG results for fabrics with flame-retardant coating before and after washes.

		PET/AC/FR	PET/AC/ FR/1	PET/AC/ FR/5	PET/AC/ FR/10	PET/AC/ FR/15
	T Onset 1, °C	264.8 ± 0.4b	343.7 ± 0.5	386.6 ± 0.9	387.7 ± 0.7	386.6 ± 1.2
Cton 1	T <sub>Max 1</sub> , °C	295.3 ± 1.2	372.6 ± 0.9	402.5 ± 0.6	399.3 ± 0.5	398.1 ± 0.7
Step 1	T End 1, °C	311.5 ± 0.9	412.0 ± 1.0	413.4 ± 0.8	410.0 ± 1.2	411.8 ± 1.2
	Residual weight, %	92.9 ± 1.1	71.1 ± 0.7	64.0 ± 1.2	70.3 ± 1.3	68.2 ± 0.4
	T Onset 2, °C	311.5 ± 0.9	412.0 ± 1.0	413.4 ± 0.8	410.0 ± 1.2	411.8 ± 1.2
Step 2	T <sub>Max 2</sub> , °C	360.7 ± 1.0	433.6 ± 0.8	432.2 ± 0.8	433.7 ± 0.9	432.4 ± 0.9
Step 2	T End 2, °C	393.7 ± 0.7	463.0 ± 1.6	461.5 ± 1.3	454.6 ± 0.9	454.1 ± 1.0
	Residual weight, %	54.7 ± 0.8	30.0 ± 0.9	17.5 ± 1.2	17.7 ± 1.4	17.5 ± 1.1
	T Onset 3, °C	393.7 ± 0.7	-	-	-	-
Step 3	T <sub>Max 3</sub> , °C	434.8 ± 1.6	-	-	-	-
	T End 3, °C	463.3 ± 0.9	-	-	-	-
	Residual weight, %	34.3 ± 0.6	-	-	-	-

ing – film (AC/FR/f) occurs in two steps with a maximum of endothermic peaks at  $296.0 \pm 2.5$  °C and  $382.2 \pm 1.8$  °C. The thermal degradation process ends at  $402.4 \pm 1.1$  °C with a weight loss of  $48.5 \pm 1.3\%$ .

The degradation of PET/AC fabric begins at a much lower initial temperature than the raw fabric (Table 9, Figure 8.b). This is due to the presence of polyacrylic coating, which degrades faster than the textile component, reducing the initial degradation temperature. A twostage process begins at 376.0 ± 1.1 °C (Table 9), which corresponds to the initial degradation temperature of the polyacrylic unmodified film (AC/f), being higher than the temperature of the crosslinked unmodified coating-film (ACH) by about 7.8 °C. The peak maximum of this step occurs at  $405.6 \pm 1.4$  °C (about 4 °C higher than  $T_{Max1}$  of AC/f). The second step begins at  $414.8 \pm 0.9$  °C and is associated with the initial degradation temperature of PET/AC fabric (Table 9), for which the T<sub>Onset</sub> is higher by 19.4 °C than the temperature for the raw fabric. The peak maximu the T<sub>m</sub> of second step  $T_{Max2}$  for the PET/AC occurs in 430.1  $\pm$ 0.3 °C and is almost comparable to the value of the T<sub>Max1</sub> for the raw fabric. The weight loss of PET/AC fabric in T<sub>End</sub> at  $472.4 \pm 0.4$  °C is 83.5%, which is higher by 2.2% than for the raw fabric.

PET/AC/FR fabric is degraded with three steps (*Table 10*, *Figure 8.b*). The first step begins at  $264.8 \pm 0.4$  °C. The second step is the main step of thermal degradation and corresponds to the degradation of the cross-linked flame-retardant coating. The third step is connected with the degradation of the textile component. For this step the initial temperature is lower by about 1.7 °C, and the temperature  $T_{Max3}$  is higher by 3.7 °C than for the raw fabric (*Table 8*). The weight loss at at the end temperature of the last step amounted to  $65.7 \pm 0.6\%$  (*Table 10*).

The results confirm those obtained by Alongi et al. [7], who observed that the thermal degradation of coated fabric proceeded at a lower temperature with less weight loss than uncoated fabric. The initial temperature of the whole composite degradation was 370 °C, which was lower by 16 °C than for PET fabric. In our work, the difference between the initial temperature for the PET/AC/FR fabric and for the raw fabric is 130.6 °C. The weight loss of uncoated and coated fabrics obtained by Alongi et al. [7] is 90% and 84%, respectively. In our case, the weight loss is 81.3% and 65.7% for the raw PET fabric and coated PET/AC/FR fabric, respectively. The reduced thermal stability of the fabric made of cotton and fireproofed polyester (PESFR/Cotton) with polyacrylic coatings with and without flame-retardants in comparison with raw PESFR/Cotton fabric was also found by Drevelle et al. [11]. The thermal degradation of coated fabrics started at 230 °C and 280 °C, respectively, which aremuch lower than for raw PESFR/Cotton fabric (300 °C). Lefebvre et al. [1], who studied the thermal properties of PETFR/Cotton fabric with polyacrylic coating and raw fabric, did not observe the influence of the coating on thermal degradation temperatures.

In our work the flame-retardants contain phosphorus. It was documented that this element acts in a condensed phase by increasing the amount of char residue, which restricts the release of gases (volatile fuels), melting and further thermal decomposition of the modified coating and modified textile material [7, 10, 11, 13 - 16].

Ten-times washing did not bring about significant changes in the TG/DTG weight loss of PET/AC fabric, which amounted to about 83% (*Table 9*, *Fig-*

ure 9.a). After the 15th wash the weight loss increased by 1.7%; the initial temperature decreased by 0.7 °C; the final temperature increased by 0.9 °C; the temperature at the maximum peak T<sub>Max1</sub> did not change, and T<sub>Max2</sub> increased by about 2 °C. In the case of PET/AC/FR fabric after the 1st wash the initial temperature increased by about 78.9 °C and the weight loss increased by 4.3% (Table 10, Figure 9.b), which indicates the partial remove of flame-retardants from the coating. After the 5th wash the weight loss increased by 16.8% and the initial temperature by 121.8 °C, similar to the sample after 15 washes (Table 10). After 5, 10 and 15 washes the peak characteristic for the flame-retardants is not observed on DTG thermograms, and characteristic peaks of PET/AC fabric degradation are present only (Figure 9.b). This indicates that the flame-retardants were already rinsed after the fifth wash, which was also found by the SEM/EDS analysis (Table 4, Figure 4).

## Conclusions

The aim of the study was to assess the thermal properties of polyester, PET, fabrics with unmodified and flame-retardant modified polyacrylic coatings after washing treatment.

The presence of polyacrylic coating resulted in a decrease in the enthalpy of phase transformation of the coated fabric as compared to the raw fabric. Multiple washing treatment of the coated fabric influenced the melting enthalpy, but the initial melting temperature of the unmodified coated fabric did not vary. Flame-retardant coating resulted in a reduction in the melting enthalpy value. Thermal decomposition starts at a lower temperature than for the unmodified coated fabric, because of the presence of flame-retardant agents. Also the melting process begins at a lower temperature in comparison with the raw fabric. The TG/DTA weight loss of the flame-retardant coated fabric before washing is much lower than for the raw and unmodified coated fabrics. The TG/DTA residual weight for the flame-retardant fabric is significantly higher in comparison to the unmodified coated fabrics corresponding to the mechanism of flame-retardant activity in the condensed phase i.e. increasing the amount of residue, thereby restricting the release of gases and thermal decomposition of the modified textile material. Washing treatment increased the initial melting temperature of the flame-retardant coated fabric. After five washes there are no signs of flame-retardants on the thermograms, which is the result of their having been rinsed out, which confirms the results of SEM/EDS analysis. Polyacrylic coatings cause a decrease in the initial thermal degradation temperature of the whole composite, especially for the flame-retardant version. The flame-retardant modification tested is not resistant to multiple washing. The techniques used may be useful for development and initial assessment of flame-retardant textile materials before testing on a bigger scale, according to suitable flammability tests.

# Acknowledgements

- The study has been carried out within the project BZT 0132 on the apparatus purchased in projects: POIG.01.03.01-00-004/08 Functional nano- and micro textile materials NANOMITEX co-financed by the European Union with the financial resources of the European Regional Development Fund and the National Centre for Research and Development and WND-RPLD.03.01.00-001/09 co-financed by the European Union with the financial resources of the European Regional Development Fund and the Ministry of Culture and National Heritage
- The authors would like to thank Ms D. Kowalczyk, Ms G. Malinowska and Ms A. Kaleta for their technical contribution in the coating process.

# References

- Lefebvre J, Le Bras M, Lefort B, Drevelle C, Duquesne S, Vouters M, Magniez C. Effect of bonding resins on the flammability properties and thermal behavior of cotton and cotton/PESFR woven fabrics. J. Ind. Text 2003; 33: 55-72.
- Xu H, Qiu F, Wang Y, Wu W, Yang D, Guo Q. UV-curable waterborne polyurethane-acrylate: preparation, characterization and properties. *Prog Org Coat* 2012; 73: 47-53.
- Pan H, Chen D. Waterborne polyurethane coating and its new applications in plush finishing. *Text. Res. J.* 2009; 79: 687-693.
- Mondal S, Hu JL, Water vapor permeability of cotton fabrics coated with shape memory polyurethane. *Carbohydrate Polymers* 2007; 67: 282-287.
- Devaux E, Rochery M, Bourbigot S. Polyurethane/clay and polyurethane/POSS nanocomposites as flame retardant

- coating for polyester and cotton fabric. *Fire Mat* 2002; 26: 149-154.
- Skoc MS, Macan J, Pezelj E. Modification of polyurethane-coated fabrics by sol-gel thin films. *Appl. Polym. Sci.* 2013. DOI: 10.1002/APP.39914.
- Alongi J, Carosio F, Malucelli G. Influence of ammonium polyphosphate-/poly(acrylic acid)-based layer by layer architectures on the char formation in cotton, polyster and their blends. *Polym. Degrad. Stab.* 2012; 97: 1644-1653.
- Drevelle C, Duquesne S, Le Bras M, Lefebvre J, Delobel R, Castrovinci A, Magniez C, Vouters M. Influence of ammonium polyphosphate on the mechanism of thermal degradation of an acrylic binder resin. *J. Appl. Polym. Sci.* 2004; 94: 717-729.
- Carosio F, Alongi J, Malucelli G. Layer by layer ammonium polyphosphatebased coatings for flame retardancy of polyester-cotton blends. *Carbohydrate Polymers* 2012; 88: 1460-1469.
- Carosio F, Alongi J, Malucelli G. Flammability and combustion properties of ammonium polyphosphate-/poly(acrylic acid)-based layer by layer architectures deposited on cotton, polyester and their blends. *Polym. Degrad. Stab.* 2013; 98: 1626-1637
- Drevelle C, Lefebvre J, Duquesne S, Le Bras M, Poutch F, Vouters M, Magniez C. Thermal and fire behavior of ammonium polyphosphate/acrylic coated cotton/ PSFR fabric. *Poly. Degrad. Stab.* 2005; 88: 130-137.
- Lecomte HA, Liggat JJ. Commercial fireretarded PET formulations-relationship between thermal degradation behavior and fire-retardant action. *Polym. Degrad. Stab.* 2008; 93: 498-506.
- Mathews MC. Durable and non-toxic topical flame retardants for cotton and cotton blends. In: *Textile Engineering*. Raleigh, North Carolina, 2007.
- Schartel B. Phosphorus-based flame retardancy mechanisms – old hat or a starting point for future development. *Materials* 2010; 3: 4710-4745.
- 15. Zhang H. Textile flame retardant review. *Mod. Appl. Sci.* 2009; 3: 129-133.
- Bisschoff J. Phosphorous flame retardants. In: Oxygenated hydrocarbon compounds as flame retardants for polyester fabric. University of Pretoria, 2000. p. 38-45.
- Received 28.01.2015 Reviewed 02.03.2015



# INSTITUTE OF BIOPOLYMERS AND CHEMICAL FIBRES

# LABORATORY OF BIODEGRADATION

The Laboratory of Biodegradation operates within the structure of the Institute of Biopolymers and Chemical Fibres. It is a modern laboratory with a certificate of accreditation according to Standard PN-EN/ISO/IEC-17025: 2005 (a quality system) bestowed by the Polish Accreditation Centre (PCA). The laboratory works at a global level and can cooperate with many institutions that produce, process and investigate polymeric materials. Thanks to its modern equipment, the Laboratory of Biodegradation can maintain cooperation with Polish and foreign research centers as well as manufacturers and be helpful in assessing the biodegradability of polymeric materials and textiles.

The Laboratory of Biodegradation assesses the susceptibility of polymeric and textile materials to biological degradation caused by microorganisms occurring in the natural environment (soil, compost and water medium). The testing of biodegradation is carried out in oxygen using innovative methods like respirometric testing with the continuous reading of the CO<sub>2</sub> delivered.



The laboratory's modern MICRO-OXYMAX RESPIROMETER is used for carrying out tests in accordance with International Standards.

The methodology of biodegradability testing has been prepared on the basis of the following standards:

- testing in aqueous medium: 'Determination of the ultimate aerobic biodegrability of plastic materials and textiles in an aqueous medium. A method of analysing the carbon dioxide evolved' (PN-EN ISO 14 852: 2007, and PN-EN ISO 8192: 2007)
- testing in compost medium: 'Determination of the degree of disintergation of plastic materials and textiles under simulated composting conditions in a laboratory-scale test. A method of determining the weight loss' (PN-EN ISO 20 200: 2007, PN-EN ISO 14 045: 2005, and PN-EN ISO 14 806: 2010)
- **testing in soil medium:** 'Determination of the degree of disintergation of plastic materials and textiles under simulated soil conditions in a laboratory-scale test. A method of determining the weight loss' (PN-EN ISO 11 266: 1997, PN-EN ISO 11 721-1: 2002, and PN-EN ISO 11 721-2: 2002).





The following methods are applied in the assessment of biodegradation: gel chromatography (GPC), infrared spectroscopy (IR), thermogravimetric analysis (TGA) and scanning electron microscopy (SEM).

### Contact:

INSTITUTE OF BIOPOLYMERS AND CHEMICAL FIBRES ul. M. Skłodowskiej-Curie 19/27, 90-570 Łódź, Poland Agnieszka Gutowska Ph. D., tel. (+48 42) 638 03 31, e-mail: lab@ibwch.lodz.pl